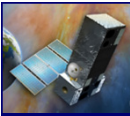




National Aeronautics  
and Space Administration  
**Jet Propulsion Laboratory**  
California Institute of Technology



**SIM Lite ASTROMETRIC OBSERVATORY**

# ***Testing of a Methane Cryogenic Heat Pipe with a Liquid Trap Turn-off Feature for Use on Space Interferometer Mission (SIM)***

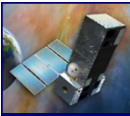
*7 March 2011*

*Juan Cepeda-Rizo, Robert Krylo, and Melanie Fisher,  
Jet Propulsion Laboratory (California Institute of Technology)*

*David C. Bugby, ATK Aerospace Systems, Beltsville, MD*

**15th CONFERENCE ON THERMOPHYSICS APPLICATIONS IN MICROGRAVITY**  
**March 7, 2011 at the Aerospace Corporation, El Segundo, CA 9009-2957**

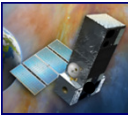
# Outline



## SIM Lite ASTROMETRIC OBSERVATORY

- ***Introduction***
- ***Concept***
- ***Trades***
- 
- ***Design***
- ***Testing***
- 
- ***Results***
- ***Conclusion***

# Introduction



## SIM Lite ASTROMETRIC OBSERVATORY

**JPL Technical Need:** In mid-2009, JPL contacted ATK and described a need for a heat transport system (HTS) to link two CCD cameras (within the Astrometric Beam Combiner (ABC) instrument on **SIM Lite**) to a cryoradiator.

**SIM Lite:** Formerly the Space Interferometry Mission (SIM), the SIM Lite Astrometric Observatory will utilize optical inteferometry to determine the positions/distances of stars much more accurately than any previous program.

### **HTS Requirements -- Normal Operation:**

- Hot-side temperature/range: 153 K / 150-156 K
- Hot-side heat load: 6-12 W
- Cold-side cooling source: 140 K cryoradiator
- Transport length: 1.4 m

### **HTS Requirements -- Decontamination:**

- Hot-side decontamination temperature: 293 K
- Hot-side decontamination heater power: Minimize

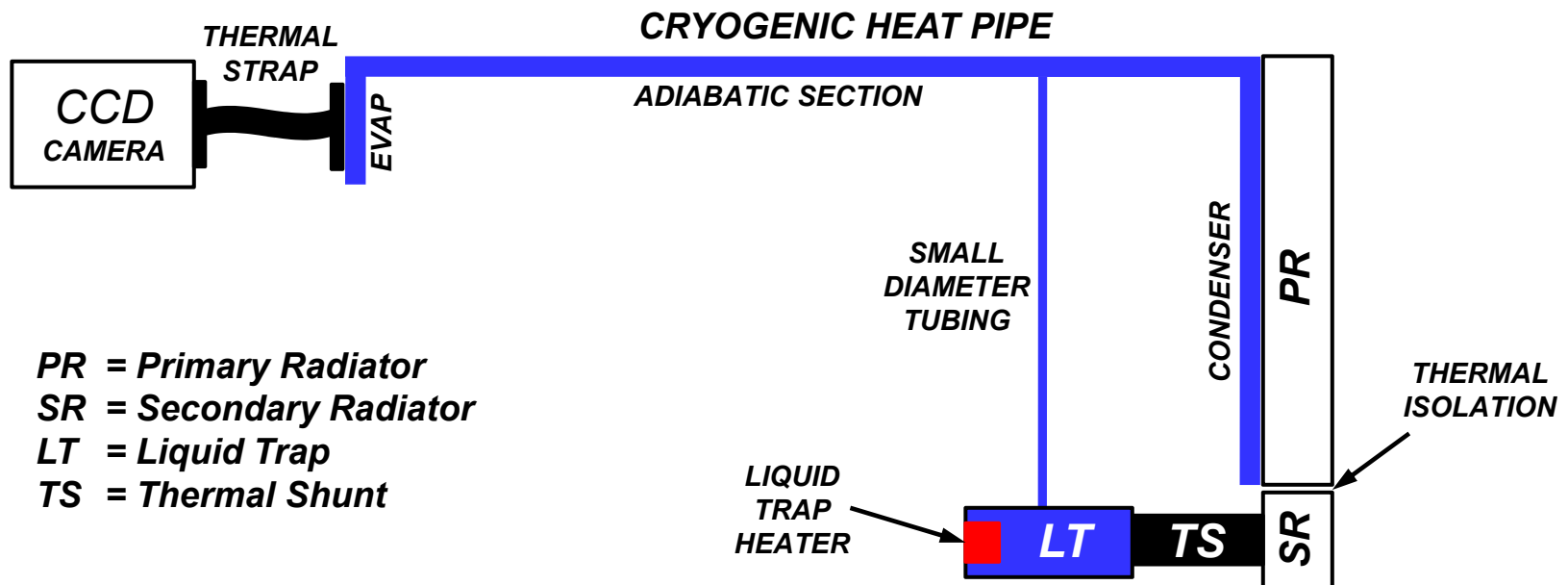
### **Additional Requirements:**

- Flight heritage: Maximize
- Cost/manufacturing complexity: Minimize

# Concept

**Solution:** Cryogenic heat pipe with thermal switching capability provided by a secondary radiator thermally isolated from the primary radiator, a thermally shunted liquid trap, and small liquid trap heater.

- During **normal operation**, the small liquid trap heater keeps the liquid trap warm enough so that it is filled with vapor only thus the heat pipe is ON.
- During **decontamination**, the liquid trap heater is turned off and all the working fluid migrates to the liquid trap turning the heat pipe OFF.





# Trades



**Working Fluid:**

**Heat pipe Architecture:**

**Flight Heritage:**

**Charge Pressure:**

**Transport Capacity:**

**Radiator Sizing:**

**Shunt Conductance:**

**Evaporator Conductance:**

**Condenser Conductance:**

**Parasitics:**

**Cooldown Time:**

**Heater Sizing:**

**Decontamination:  
power**

**Switching Time:**

**Static Height:**

**Structural Analysis:**

**Testing:**

*ethane vs. methane*

*axial groove vs. non-axial groove*

*CRISM vs. other methane HP flight systems*

*ambient tank vs. high pressure heat pipe*

*large diam./margin vs. small diam./margin*

*large area, fast test vs. small area, slow test*

*high G, speed, power vs. low G, speed, power*

*6" length specified by JPL vs. shorter/longer*

*28" length specified by JPL vs. shorter/longer*

*environment induced vs. heater induced*

*small A, slow cooling vs. large A, fast cooling*

*ground testing ease vs. system optimization*

*high power vs. moderate power vs. low*

*fast, high G shunt vs. slow, low G shunt*

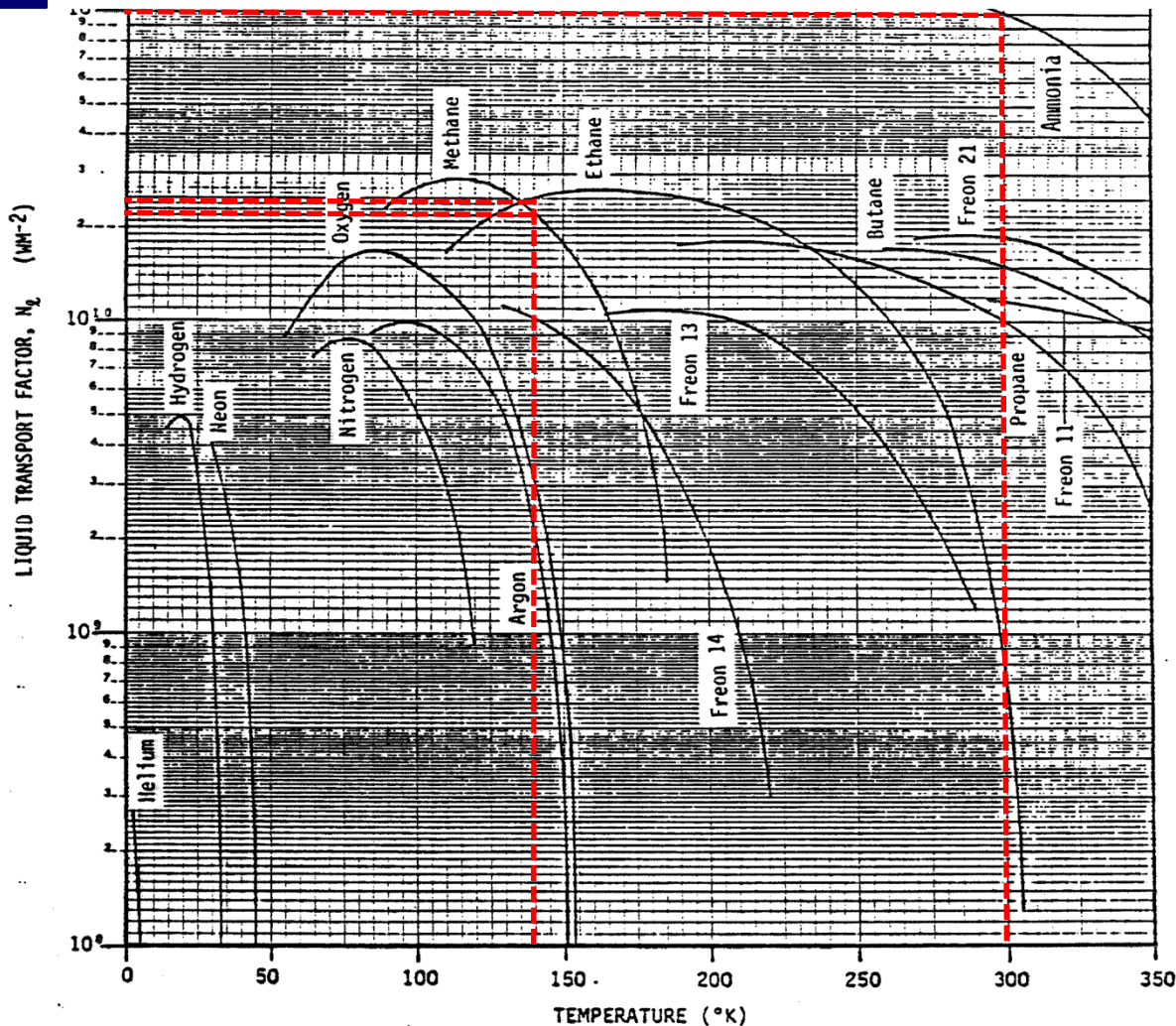
*small diam., 1-g < 0-g vs. large diam. 1-g > 0-g*

*low mass, margin vs. high mass, margin*

*minimum needed vs. extensive verification*

# Trades

## Working Fluid



Two possible working fluid choices for a heat pipe with a 140 K radiator (vapor) temperature are **methane** and **ethane**.

At this temperature, the liquid transport factor ( $N_L$ ) of methane and ethane are about equal and about 1/5 of that of ammonia at 300 K.

Upon (decontamination) heating, methane liquid transport factor decreases whereas ethane liquid transport factor increases .... thus, an ethane HP will require much more heater power before dry-out occurs, making **methane a better choice than ethane**.

$$N_L = \frac{\sigma \Delta H}{v}$$



# Design

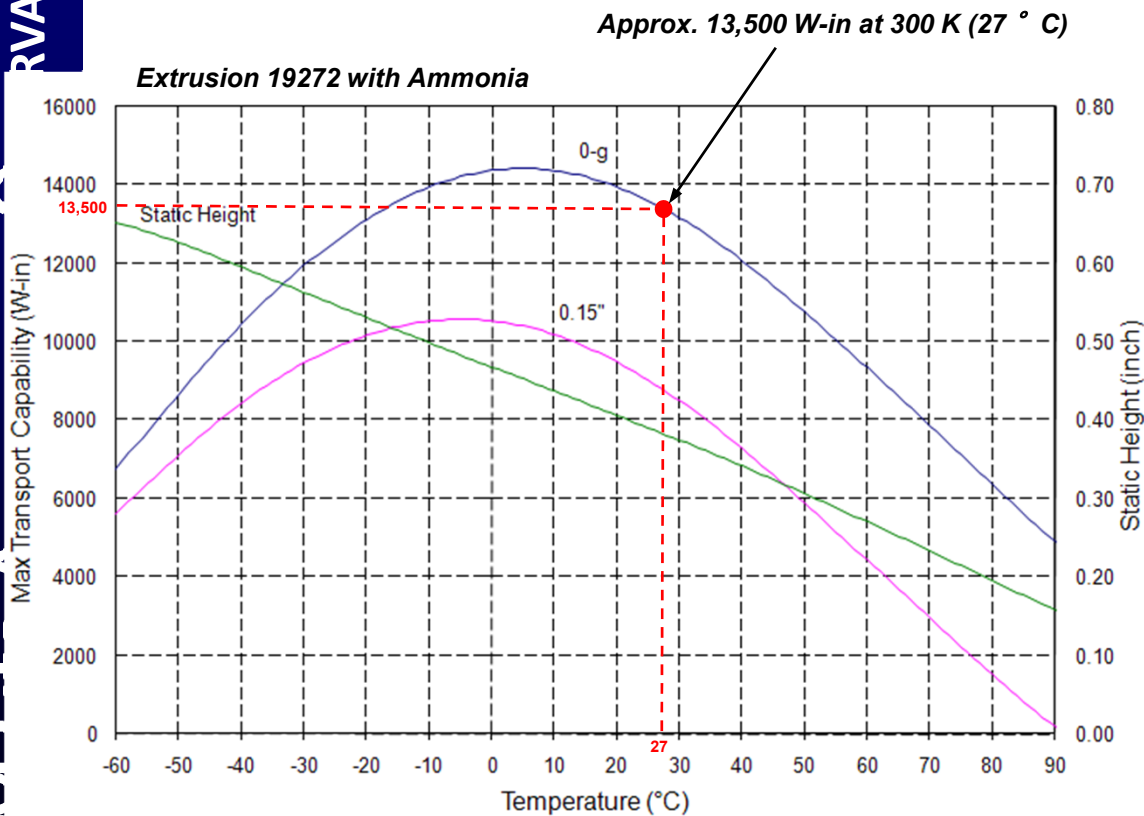
## Transport Capacity

**Requirement:**  $QL = (12 \text{ W max load} + 2 \text{ W parasitics}) * 73.5'' \text{ effective length} = 1029 \text{ W-in}$

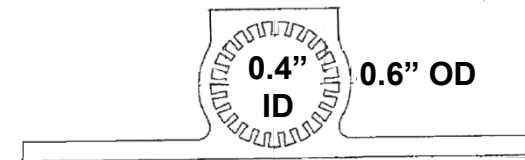
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## Extrusion 19272



Transport capacity with methane at 140 K ~ 22% the transport capacity of ammonia at 300 K or **2970 W-in**, which provides almost 200% margin on the QL requirement of 1029 W-in.

Analytical estimate of methane transport capacity at 140 K with this extrusion is **3188 W-in**.

# Design

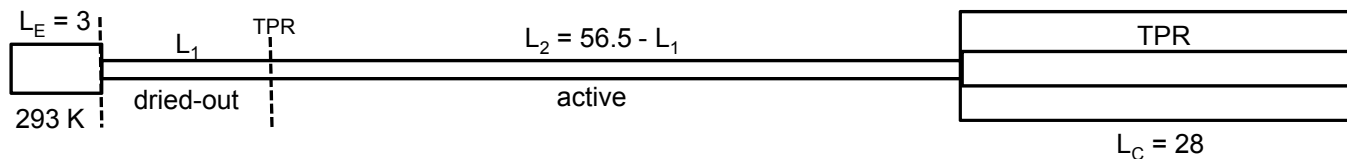
## Decontamination

### Option 1: *High Power* ( $Q \sim 120\text{ W}$ )

- Heat primary radiator (PR) above methane critical temperature (191 K)
- Heat evaporator to 293 K (heat pipe all vapor)
- Maintain heater power on liquid trap; keep above primary radiator temperature

### Option 2: *Medium Power* (40 W)

- Heat evaporator to 293 K (evaporator dries out; part of heat pipe still works)
- Maintain heater power on liquid trap; keep above primary radiator temperature



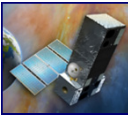
### Option 3: *Minimum Power* (3 W)

- Turn liquid trap heater OFF
- Heat evaporator to 293 K (heat pipe evacuated by trap)





# Test Outline



## **1. Initial cooling – Day 1**

## **2. Methane Radiator Test** - (to establish Stefan-Boltzmann constant $\epsilon \cdot A \cdot \cos \theta$ factor from the surface). Remove temperature control from the condenser.

High Power at evaporator

Nominal Power at evaporator

Low Power at evaporator

## **3. Heat Pipe Characteristic Test** - Control the condenser radiator to a fixed temperature. Apply a heat load to the evaporator. Do several cases for several condenser temperatures.

Low condenser temp, low evaporator power

Nom. condenser temp, low evaporator power

Nom. condenser temp, nominal evaporator power

High condenser temp, low evaporator power

High condenser temp, nominal evaporator power

High condenser temp, high power – Day 2

## **4. System Test** - Remove temperature control from the condenser radiator. Apply heat to the evaporator. Measure the evaporator temperature and condenser temperature

Low Power

Nominal Power

High Power

## **5. Turn-off with hot radiator**

## **6. Decontamination -1 – Day 3**

## **7. Cool down to nominal - Day 4**

## **8. Turn-off with liquid trap – Day 5**

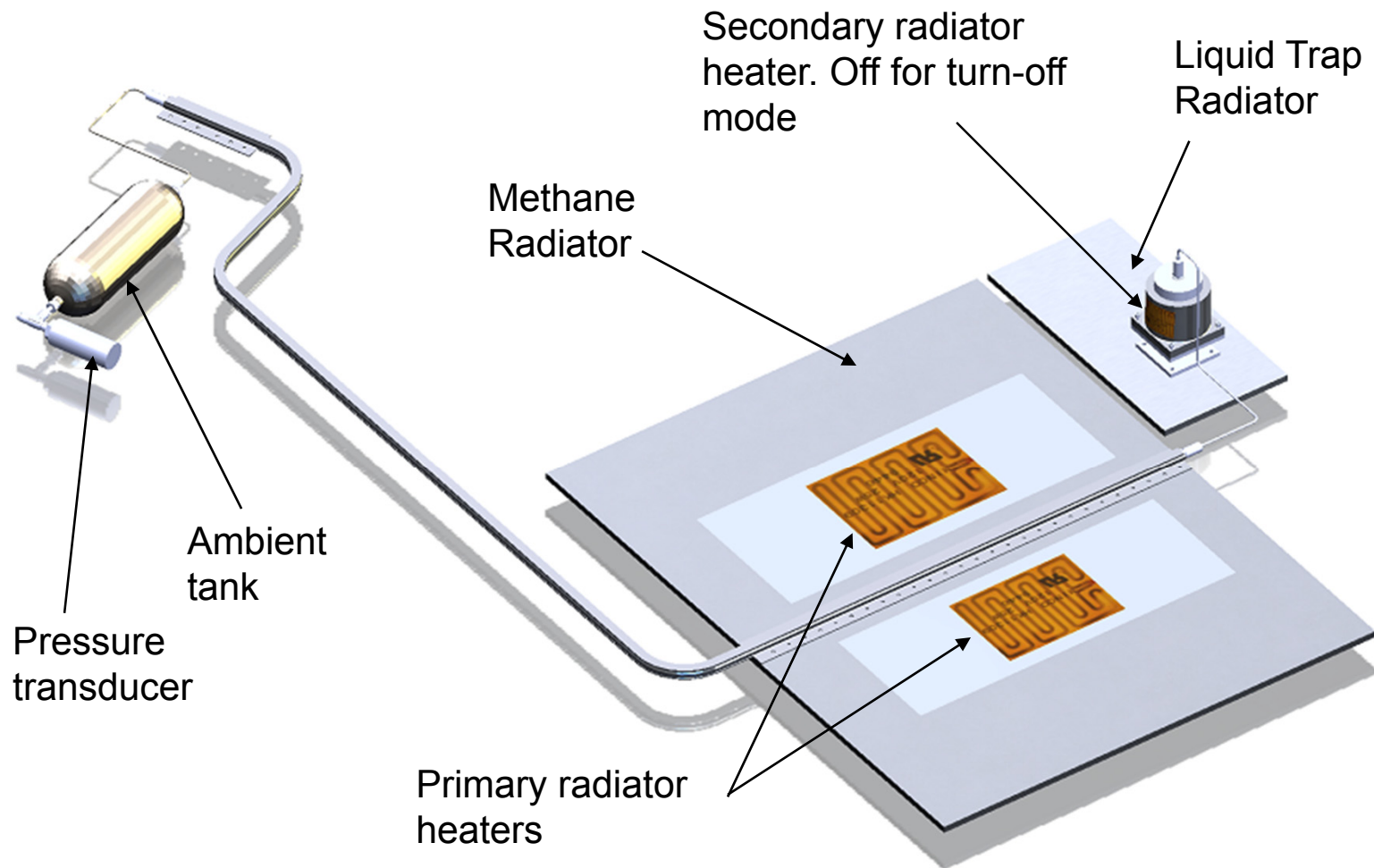
## **9. Decontamination -2**

## **10. End of test**

# Heat Pipe with Radiators

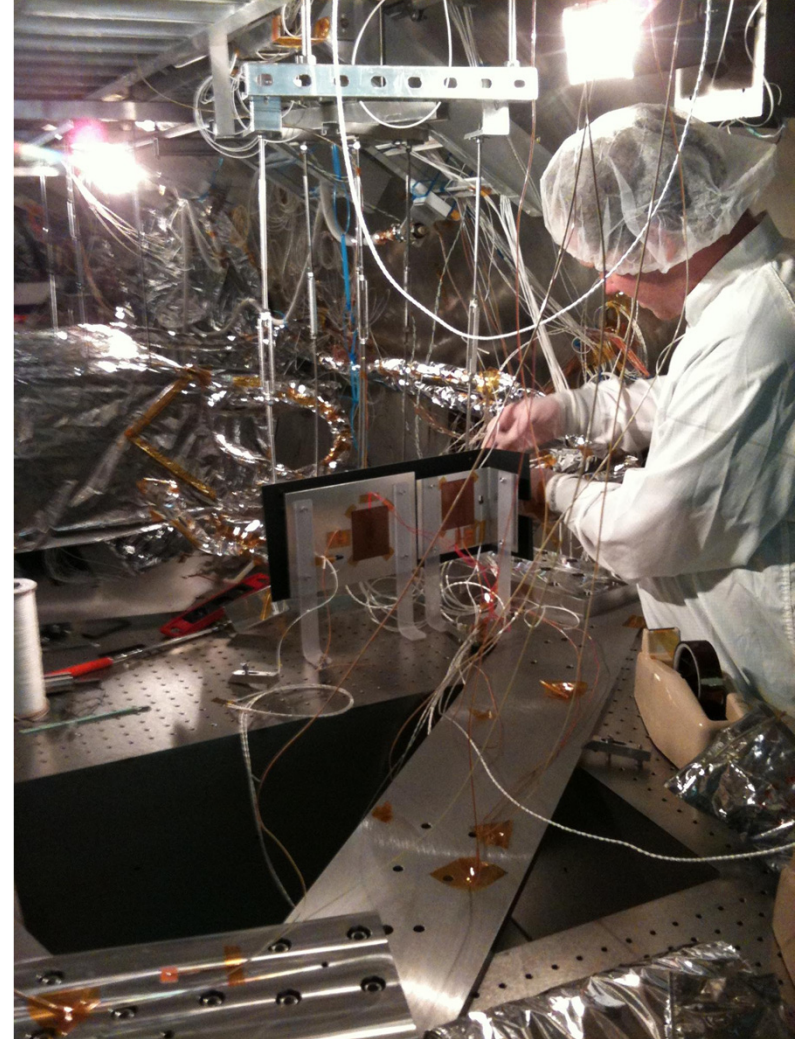
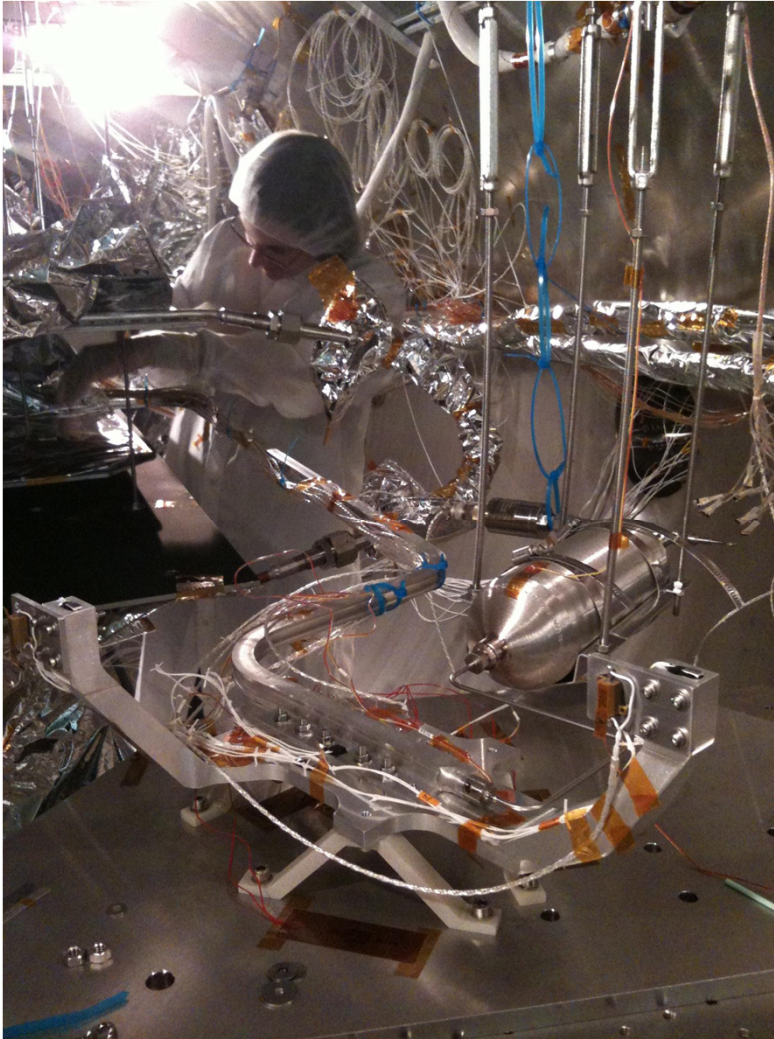


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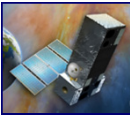
# Test Fixture Assembly

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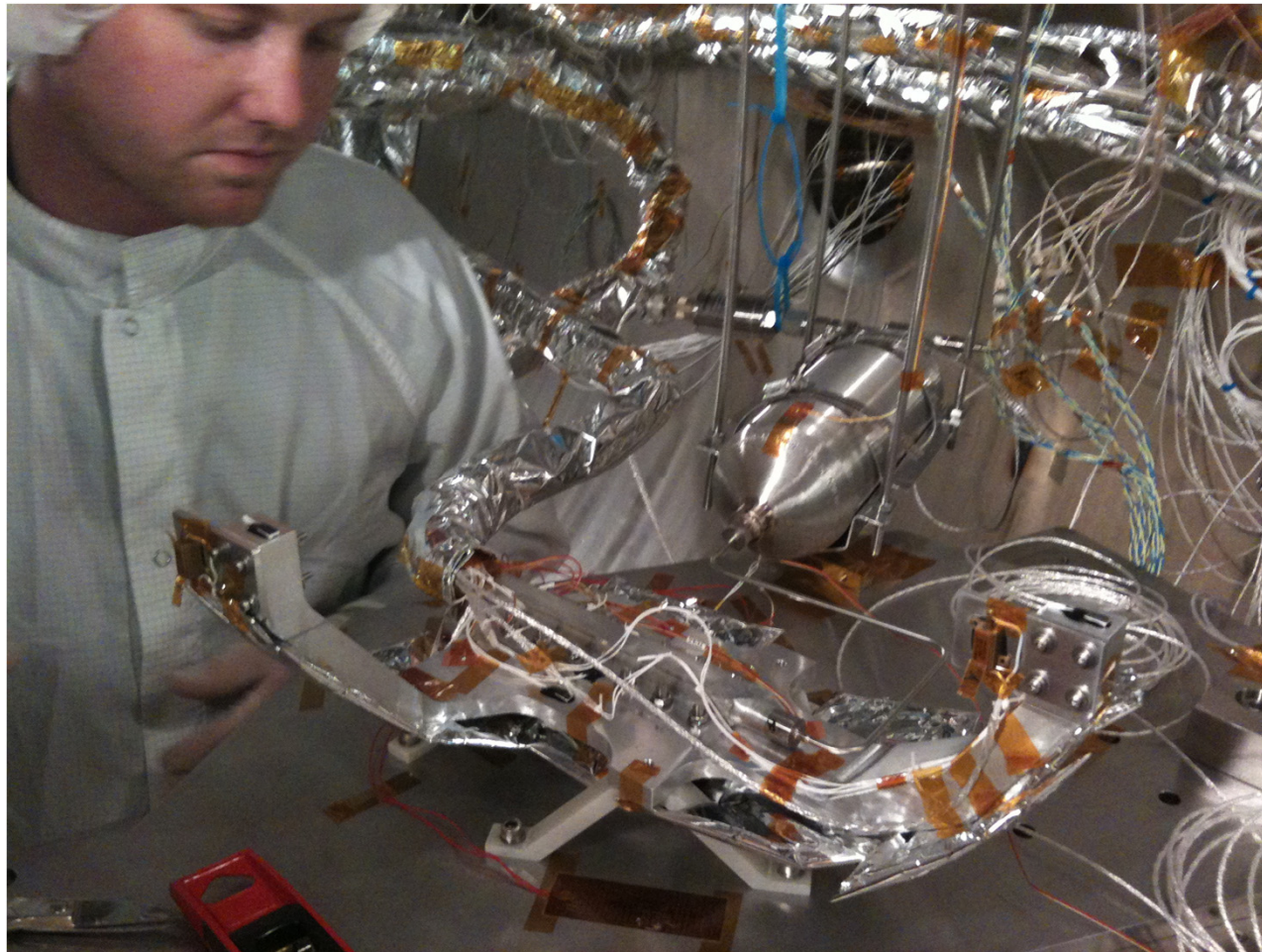




# Test Fixture Assembly - Evaporator

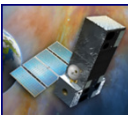


**SIM Lite ASTROMETRIC OBSERVATORY**



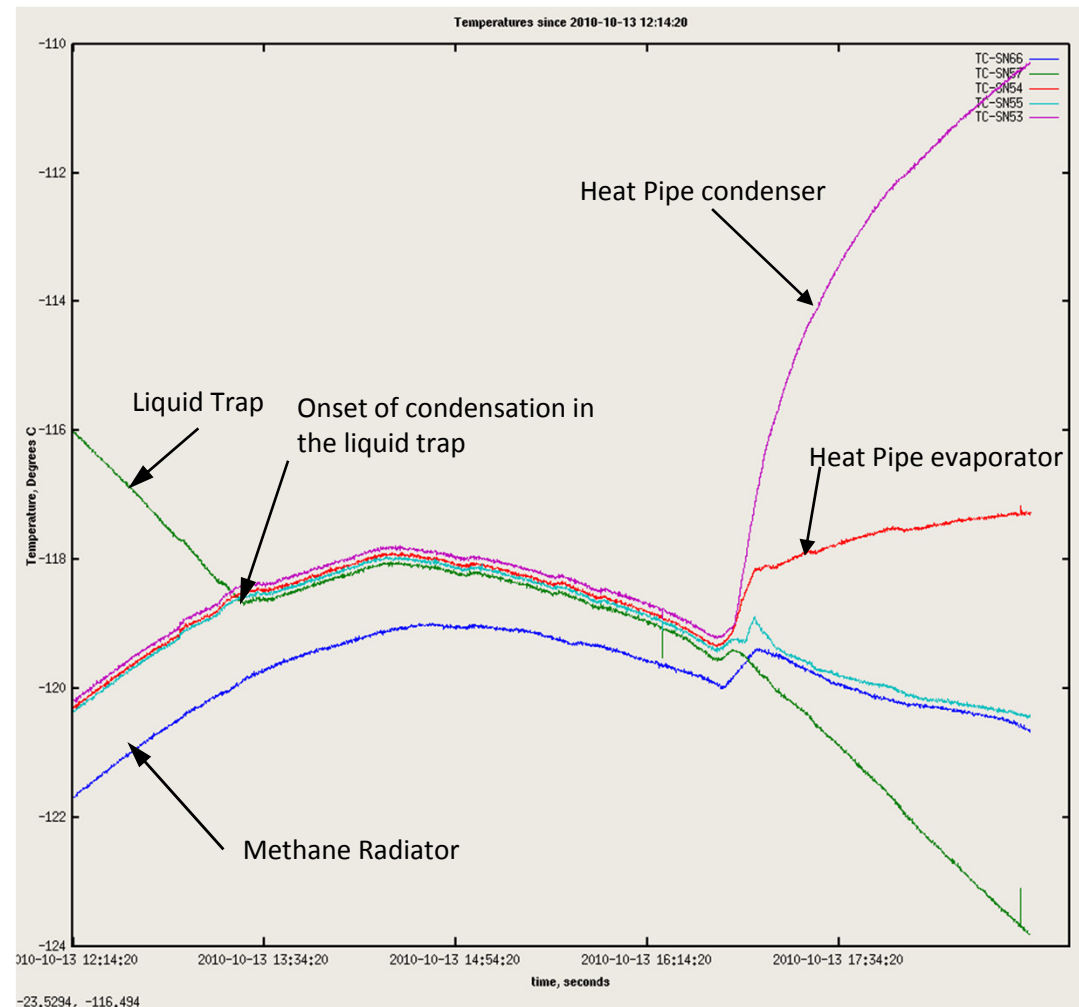


## Heat Pipe Test Data, Step 2, Shut-Off Transient

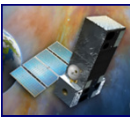


### SIM Lite ASTROMETRIC OBSERVATORY

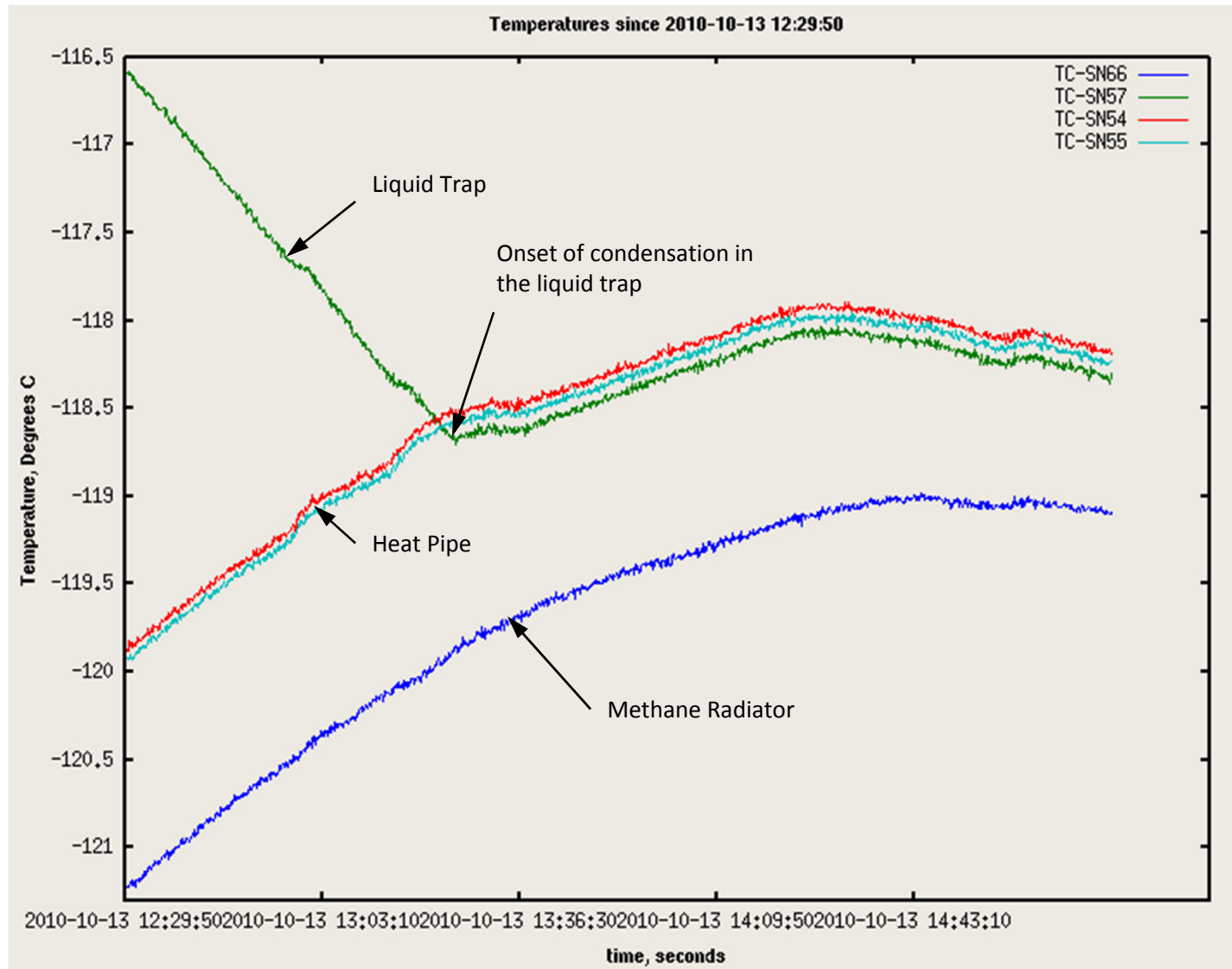
- The green line is the liquid trap. The trap cools to roughly -119C where the methane starts condensing. The magenta line is the condenser of the pipe, warming under the influence of a heater. Both items operate at the saturation temperature during the shut-down transient. It takes about 4hrs for the trap to condense the methane and dry the pipe. Then the temperatures diverge and the trap cools while the heater continues to warm the condenser.



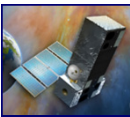
## Heat Pipe Test Data, Step 2, Shut-Off Transient



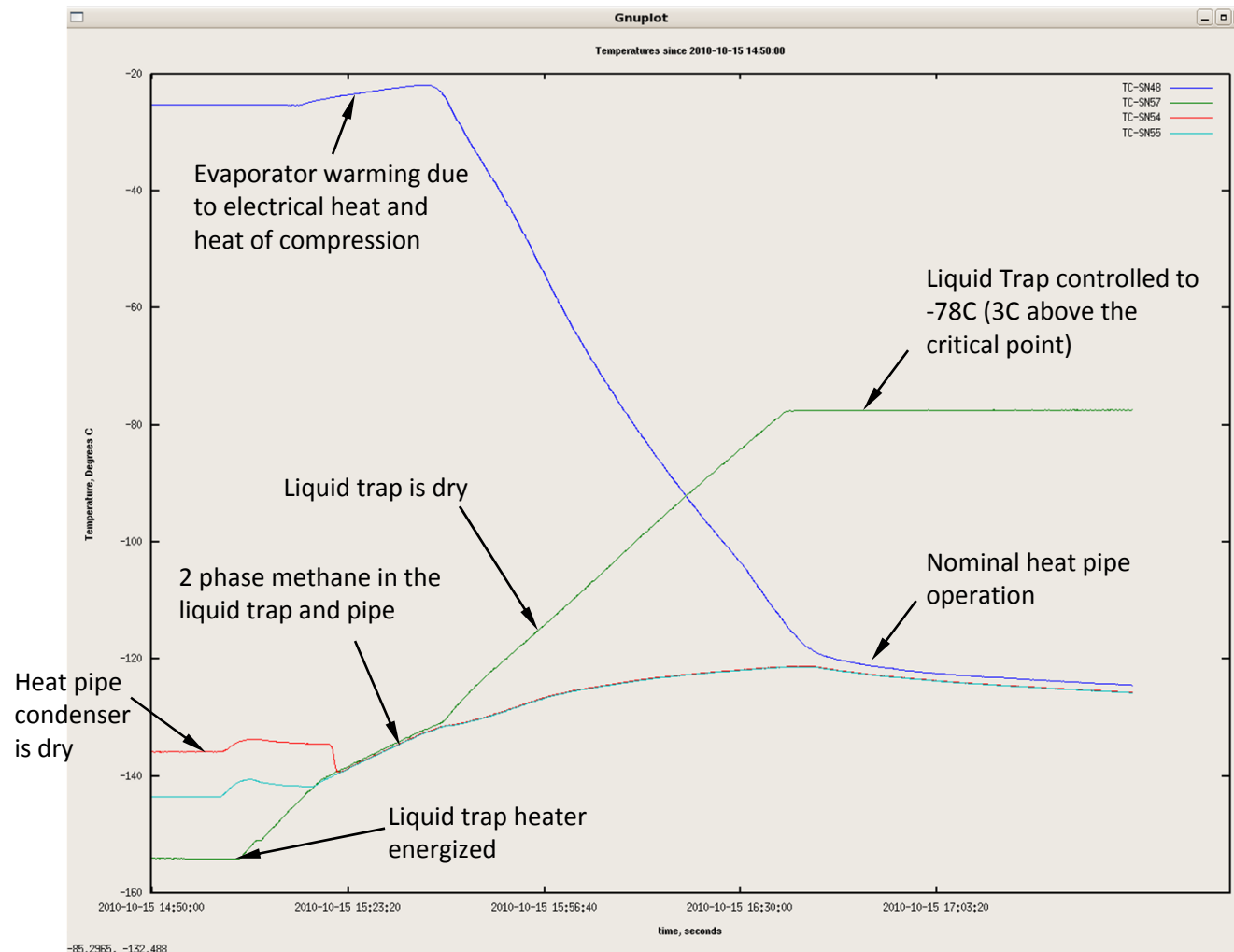
SIM Lite ASTROMETRIC OBSERVATORY



# Heat Pipe Test Data, Step 5, Turn-On and Cooling

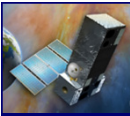


SIM Lite ASTROMETRIC OBSERVATORY





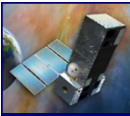
## Conclusion



### SIM Lite Astrometric Observatory

- Camera cooling for SIM presents three thermal control challenges; stable operation at 163K ( $-110^{\circ}$  C), decontamination heating to  $+20^{\circ}$  C, and a long span from the cameras to the radiator. A novel cryogenic cooling system based on a methane heat pipe meets these challenges.
- The SIM thermal team, with the help of heat pipe vendor ATK, designed and tested a complete, low temperature, cooling system. The system accommodates the two SIM cameras with a double-ended conduction bar, a single methane heat pipe, independent turn-off devices, and a flight-like radiator. The turn-off devices consist of a liquid trap, for removing the methane from the pipe, and an electrical heater to raise the methane temperature above the critical point thus preventing two-phase operation.
- This is the first time a cryogenic heat pipe has been tested at JPL and is also the first heat pipe to incorporate the turn-off features. Operation at 163K with a methane heat pipe is an important new thermal control capability for the lab. In addition, the two turn-off technologies enhance the “bag of tricks” available to the JPL thermal community. The successful test program brings this heat pipe to a high level of technology readiness.

# Lessons Learned



## During Procurement

- To save money, we chose to build our own test fixture to hold heat pipe in place during test.
  - Too much improvising required. It took us many days to of chamber time to configure our fixture just right. We also probably put the hardware at risk of damage, especially rupturing of the thin-walled tubing connecting heat pipe to liquid trap and ambient tank.

## During Test

- Establish realistic steady-state criterion upfront. We used one K/hr, but we had to “tighten” or requirement because we saw constant drift upwards that made us feel uncomfortable with declaring steady-state reached.
- Getting to cold temperature steady-state usually takes longer than you think.
- CCD Electronic boxes were not designed for operation in a vacuum, so they heated up. They had to be cycled off and on manually to avoid overheating

# SIM Thermal Design and Test Team

- Melanie Fisher, Bob Krylo, and Juan Cepeda-Rizo



SIM Lite ASTROMETRIC OBSERVATORY